# NSWCCD-SIG-96/060-7030 A Double-Sum Technique for Performing a Fourier Transformation on an Integrand Composed of Aliased Factors

## Carderock Division Naval Surface Warfare Center

Bethesda, Maryland 20084-5000

NSWCCD-SIG-96/060-7030 May 1996 Signatures Directorate Research and Development Report

# A Double-Sum Technique for Performing a Fourier Transformation on an Integrand Composed of Aliased Factors

by

G. Maidanik K.J. Becker

DTIC QUALITY INSPECTED &



Approved for public release; Distribution is unlimited.

19961015 019

### SECURITY CLASSIFICATION OF THIS PAGE

REPORT DOCUMENTATION PAGE							Form Approved OMB No. 0704-0188		
1a. REPORT SECURITY CLASSIFICATION Unclassified				1b. RESTRICTIVE MARKINGS None					
2a. SECURITY CLASSIFICATION AUTHORITY				3. DISTRIBUTION / AVAILABILITY OF REPORT Approved for public release.					
2b. DECLASSIFICATION/DOWNGRADING SCHEDULE				Distribution is unlimited.					
4. PERFORMING ORGANIZATION REPORT NUMBER(S) NSWCCD-SIG-96/060-7030				5. MONITORING ORGANIZATION REPORT NUMBER(S)					
6a. NAME OF PERFORMING ORGANIZATION			6b. OFFICE SYMBOL (If applicable)	7a. NAME OF MONITORING ORGANIZATION					
NSWC, Carderock Division			Code 7030						
	(City, State, and MD 20084	•		7b. ADDRESS (City, State, and ZIP Code)					
8a. NAME OF F ORGANIZA	FUNDING/SPONS ATION	SORING	8b. OFFICE SYMBOL 9. PROCUREMENT INSTRUMENT IDENTIFICATION NUMBE (If applicable)			ON NUMBER			
8c. ADDRESS	(City, State, and	I ZIP Code)		10. SOURCE OF FUNDING NUMBERS					
				PROGRAM ELEMENT NO.	PROJECT NO.	TASK NO.	WORK UNIT ACCESSION NO.		
12. PERSONAI G. Maidan 13a. TYPE OF Research	L AUTHOR(S) ik and K.C REPORT & Developr	J. Becker 13b. TIME ment FROM 96	g a Fourier Transfor  COVERED  50101 TO 960531	14. DATE OF REPC	DRT <i>(Year, Month, Da<sub>j</sub></i> 6 May 31		. PAGE COUNT 20		
16. SUPPLEM	ENTARY NOTAT	ION							
17.	COSATI	· · · · · · · · · · · · · · · · · · ·	18. SUBJECT TERMS Structural Acou	S (Continue on reverse if necessary and identify by block number)					
FIELD	GROUP	SUB-GROUP	Wave Propagation						
19. ABSTRACT (Continue on reverse if necessary and identify by block number)  Structural acoustics often utilizes Fourier transformation to either reveal a phenomenon that is more directly recognized in one domain than in its Fourier conjugate domain or to employ complementarity in order to decipher a phenomenon. In this paper, a novel computational technique is introduced. This technique advantageously performs this transformation in situations in which specific spatial scales govern aliased factors in the integrand of a Fourier transformation. The technique can factorially save computational steps over corresponding computations that employ discrete Fourier transform procedures.  20. DISTRIBUTION / AVAILABILITY OF ABSTRACT  Sunctassified/UNCLASSIFIED/UNLIMITED SAME AS RPT. DICCUSERS Unclassified  22b. TELEPHONE (Include Area Code) 22c. OFFICE SYMBOL									
Maidanik,		INDIVIDUAL		1	E (Include Area Code) 227−1292	22¢. O	NSWCCD 7030		
	-0.			(301)	CC 1 - 1636	1	MOMCCD 1000		

### **CONTENTS**

		Page
ABS	STRACT	1
I.	INTRODUCTION	1
II.	FORMALISM OF A DOUBLE-SUM COMPUTATIONAL PROCEDURE	6
III.	INTEGRAND COMPOSED OF ALIASED FACTORS	9
REI	FERENCES	14

### **ABSTRACT**

Structural acoustics often utilizes Fourier transformation to either reveal a phenomenon that is more directly recognized in one domain than in its Fourier conjugate domain or to employ complementarity in order to decipher a phenomenon. In this report, a novel computational technique is introduced. This technique advantageously performs this transformation in situations in which specific spatial scales govern aliased factors in the integrand of a Fourier transformation. The technique can factorially save computational steps over corresponding computations that employ discrete Fourier transform procedures.

### I. INTRODUCTION

Structural acoustics deals largely with the description of wave propagations in structures and in the fluids that are in contact with their internal and external surfaces. Models of the structure are constructed so that they facilitate the derivation of these descriptions. A description may be more readily derived when the model is idealized and adapted to accommodate a given Fourier domain. Yet a phenomenon in the description may be, in some cases, more advantageously interpreted in a domain that is a Fourier conjugate to that in which the description is originally derived. Moreover, a complementary description of this kind is itself of considerable benefit in the interpretation of a phenomenon in the description. In this sense, one is often called upon to perform Fourier transformations in structural acoustics. The purpose of this report is to propose a novel computational technique to accomplish a certain class of Fourier transformations. It transpires that a number of phenomena in structural acoustics are featured in this class; in particular, those phenomena that are related to aliasing and to pass and stop bands in regularly ribbed structures [1-11].

A typical Fourier transform in this report is expressed

$$f(x,\omega) = (2\pi)^{-1/2} \int dk \ exp(-ixk) \ F(k,\omega) , \qquad (1a)$$

$$F(k,\omega) = (2\pi)^{-1/2} \int dx \ exp(ixk) \ f(x,\omega) , \qquad (1b)$$

where the k-domain and the x-domain are Fourier conjugate domains; (k) and (x) are a Fourier variable pair; and  $(\omega)$  is a silent variable in these transformations. For these equations to be valid,  $F(k,\omega)$  and  $f(x,\omega)$  need to be well behaved functions of (k) and (x), respectively, so that convergence can be guaranteed. In this report the concern is mainly focused on Eq. (1a). Using the self-aliased wavenumber operator  $S_b(k)$ , Eq. (1a) may be cast in the form

$$f(x,\omega) = (2\pi)^{-1/2} \int_{0}^{\kappa_{1}} dk \ S_{b}(k) \left\{ exp(-ixk) F(k,\omega) \right\} ;$$
 
$$\kappa_{1} = (2\pi)/(b) . \tag{2a}$$

The self-aliased wavenumber operator  $S_b(k)$  is defined

$$S_b(k) \{N(k,\omega)\} = \sum_q N(k+\kappa_q,\omega) = M(k,\omega) = M(k+\kappa_j,\omega);$$

$$S_b(k) \{K(k,\omega) | G(k,\omega)\} = K(k,\omega) | S_b(k) \{G(k,\omega)\}, \text{ if }$$

$$K(k,\omega) = K(k+\kappa_i,\omega) , \qquad (3)$$

where (b) is an appropriately selected spatial scale factor,

$$\kappa_q = q\kappa_1; \qquad \kappa_j = j\kappa_1; \qquad \kappa_1 = (2\pi/b), \qquad (4)$$

and  $N(k,\omega)$ ,  $K(k,\omega)$ , and  $G(k,\omega)$  are arbitrary but well behaved functions of the wavenumber (k). The quantities  $K(k,\omega)$ , by definition, and  $M(k,\omega)$ , by construction, are aliased; i.e., once  $K(k,\omega)$  and  $M(k,\omega)$  are specified in a segment that spans the width  $(\kappa_1)$  in the k-domain, they are specified, by repetitive extrapolation, throughout that domain. In particular, if  $K(k,\omega)$  and  $M(k,\omega)$  are known within the segment  $0 \le k < \kappa_1$ , they are known throughout the k-domain. Equation (1a) is transformed into Eq. (2a) by constructing an integrand that is "aliased in (k) with respect to  $(\kappa_1)$ " and, therefore, the integral over a single segment  $(\kappa_1)$  wide suffices; all the information that is in  $\{exp(-ixk)\ F(k,\omega)\}$  over the entire k-domain is concentrated in  $S_b(k)$   $\{exp(-ixk)\ F(k,\omega)\}$  over the segment  $0 \le k < \kappa_1$  of that domain. After the aliased integrand is sampled in this segment, the integration over this segment may be evaluated adaptively or otherwise. Alternatively, the segmental span  $(\kappa_1)$  may be chosen to be  $(\kappa_1')$  which is small enough so that a "mean value theorem" can be relied upon to evaluate the integral in Eq. (2a). At this stage, the alternative procedure is selected for the evaluation of Eq. (2a); namely

$$f(x,\omega) = (2\pi)^{-1/2} (\kappa'_1) S_{b'}(k_o) \{exp(-ixk_o) F(k_o,\omega)\};$$

$$\kappa'_1 = (2\pi/b'); \qquad k_o = (\alpha\kappa'_1);$$

$$S_{b'}(k) \{N(k,\omega)\} = \sum_{a} (N + \kappa'_q, \omega); \qquad \kappa'_q = q\kappa'_1, \qquad (2b)$$

where  $(\alpha)$  is a positive constant less than unity. [cf. Eqs. (3) and (4).] To define "small enough," the details in the integrand in Eq. (1a) may be conveniently typified by a wavenumber  $(k_{\gamma})$  and a loss factor  $(\eta_{\gamma})$ . The wavenumber  $(k_{\gamma})$  locates the position of the  $(\gamma)$ th detail and  $(\eta_{\gamma})$  estimates the extent of that detail in the k-domain. In order to capture all relevant details in this integrand, when Eq. (1a) is converted into Eq. (2b), it is necessary to impose

$$\kappa_1' << (\eta_\gamma k_\gamma) , \qquad (5)$$

for all relevant  $\gamma$ 's. Indeed, under the condition stated in Eq. (5), and after carrying out the operation dictated by  $S_{b'}(k_o)$  in Eq. (2b),  $(k_o)$  can be safely set equal to zero by choosing  $(\alpha)$  to be zero. In this limit, Eq. (2b) becomes a Fourier series expansion for  $f(x,\omega)$ . Clearly, the infinite summation that is dictated in Eq. (2b) by the operator  $S_{b'}(k_o)$  cannot be met in practice; the summation needs to be truncated. To ensure that the truncated terms can be discarded, a maximum wavenumber  $(k_M)$  is defined so that the convergence of  $F(k,\omega)$  is substantially completed when this wavenumber is reached. A number (J') is then defined and it is required that

$$f(x,\omega) \simeq (2\pi)^{-1/2} (\kappa_1') S_{b'}^{J'}(k_o) \{exp(-ixk_o) F(k_o,\omega)\};$$

$$k_M = (J'\kappa_1') , \qquad (2c)$$

constitutes an adequate approximation to Eq. (2b), where

$$S_{b'}^{J'}(k) \{N(k,\omega)\} \sum_{j=-J'}^{J'} N(k+\kappa'_j,\omega); \qquad \kappa'_j = (j\kappa'_1) . \qquad (6)$$

[cf. Eqs. (2b) and (3).] How can an adequate approximation be defined in the context of Eq. (2c)? For this purpose one needs to specify the expected "overall spatial span"  $(x_M)$  and the "spatial sampling span"  $(x_1')$  for the Fourier transform  $f(x,\omega)$ . The specification of these spatial parameters defines a number  $(J_x')$  given by

$$x_M = (J_x' x_1') . (7a)$$

The uncertainty principle and sampling theory relate  $\{k_M, \kappa_1'\}$  to  $\{x_M, x_1'\}$  in the form

$$(x_1' k_M) = (x_M \kappa_1') \ge 2\pi ; J_x' = J' \ge 2\pi (x_1' \kappa_1')^{-1} . (7b)$$

Summarizing Eqs. (2) through (7) yields

$$f(x,\omega) \simeq (2\pi)^{-1/2} (\kappa'_1) S_{b'}^{J'}(k_o) \{ exp(-ixk_o) F(k_o,\omega) \} ;$$

$$k_o = (\alpha \kappa_1') , \qquad (8)$$

and the approximation is adequate, provided

$$(\eta_{\gamma})^{-1} \ll (k_{\gamma}/\kappa_1') \ll J'; \qquad J' = (k_M/\kappa_1') = (x_M/x_1'), \quad (9)$$

is satisfied, where  $(k_{\gamma})$  and  $(\eta_{\gamma})$  define all details in  $F(k,\omega)$  in the k-domain that need to be captured to render  $f(x,\omega)$  a reliable Fourier transform. Usually  $(x'_1 \kappa'_1)$  is selected as small compared with unity and  $(\alpha)$  is selected as zero. Choosing the equality sign in Eq. (7b) and, as such, substituting it in Eq. (8), the resulting equation can be readily manipulated to conform with the discrete Fourier transform. The discrete Fourier

transform is the basis for the formulation of the Fast Fourier Transform (FFT) computational procedures [12]. In this report, however, a different computational path is selected.

### II. FORMALISM OF A DOUBLE-SUM COMPUTATIONAL PROCEDURE

The approximation that underlies Eq. (8) requires Eq. (9) to be satisfied. The latter equation implies that some knowledge of  $F(k,\omega)$  is on hand in that the various vectors  $\{k_{\gamma},\eta_{\gamma}\}$  that typify details in this function can be reasonably estimated. These estimations are then used to determine the vector  $\{\kappa'_{1},J'\}$  that needs to be imposed on Eq. (8). This vector, in turn, determines the "wavenumber sampling span"  $(\kappa'_{1})$  and the "overall wavenumber span"  $k_{M}=(J'\kappa'_{1})$ . The first determines the separation between adjacent sampling positions and the second ensures convergence. Situations may arise in which the wavenumber sampling span is selected, for some reason, to be  $(\kappa_{1})$  instead of  $(\kappa'_{1})$  and  $(\kappa_{1})>(\kappa'_{1})$ . Were this selection of  $(\kappa_{1})$  for  $(\kappa'_{1})$  to be made, what modification needs to be instituted in Eq. (1a) to bring in a finite summation, while ensuring that an adequate approximation is installed? Indeed, the approximation is required to match the accuracy that is enjoyed by Eq. (8) when this equation is covered by the imposition of Eq. (9).

Using the self-aliased operator  $S_b(k)$ , Eq. (1a) may be recast in the form

$$f(x,\omega) = (2\pi)^{-1/2} \int_{0}^{\kappa_1} dk \ S_b(k) \left\{ exp(-ixk) \ K(k,\omega) \ G(k,\omega) \right\};$$

$$\kappa_1 = (2\pi/b), \qquad (10a)$$

where, for the sake of flexibility,  $F(k, \omega)$  is expressed in the factorial form

$$F(k,\omega) = K(k,\omega) G(k,\omega) . (11)$$

[cf. Eq. (2a).] Ensuring the convergence of  $F(k,\omega)$  by an overall wavenumber span  $k_M = J\kappa_1$ , the infinite summation implied by  $S_b(k)$  is then replaced by a finite summation; namely, Eq. (10a) is approximated in the form

$$f(x,\omega) \simeq (2\pi)^{-1/2} \int_{0}^{\kappa_{1}} dk \ S_{b}^{J}(k) \left\{ exp(-ixk) \ K(k,\omega) \ G(k,\omega) \right\};$$
 
$$k_{M} = (J\kappa_{1}), \qquad (10b)$$

where

$$S_b^J(k) \{N(k,\omega)\} = \sum_{j=-J}^J N(k+\kappa_j,\omega); \qquad \kappa_j = j\kappa_1;$$
  
$$\kappa_1 = (2\pi/b), \qquad (12a)$$

[cf. Eqs. (2c) and (6).] With the help of Eq. (7) it emerges that the approximation in Eq. (10b) matches that in Eq. (2c) provided the equalities and the inequality

$$x_1 = x_1';$$
  $x_M = J'x_1;$   $k_M = (J'\kappa_1') = (J\kappa_1);$  
$$J \ge 2\pi (x_1\kappa_1)^{-1},$$
 (13)

are maintained. Since the new wavenumber sampling span  $(\kappa_1)$  is larger than the old wavenumber sampling span  $(\kappa'_1)$ , the integral cannot be evaluated by a single segment in the manner of Eq. (2c). Each segment in the summation needs to be spanned more finely. In this vein, the integral is carried out over (1+R) regular intervals, notwithstanding that an adaptive procedure may, under certain circumstances, be preferred. Executing the integral in the manner just specified, one derives from Eq. (10b) the Fourier transform in the form

$$f(x,\omega) \simeq (2\pi)^{-1/2} \ (1+R)^{-1} \ (\kappa_1) \ \sum_{r=o}^R \ S_b^J(k_r) \ \{exp(-ixk_r) \ K(k_r,\omega) \ G(k_r,\omega)\} \ ;$$

$$k_M = (J\kappa_1) \; ; \qquad k_r = (1+R)^{-1} \; \kappa_r \; ; \qquad \kappa_r = (r\kappa_1) \; ; \qquad \kappa_1 = (2\pi/b) \; .$$
 (14)

The "effective" wavenumber sampling span in Eq. (14) is then given by  $(1+R)^{-1}$   $\kappa_1$ . Using Eqs. (9) and (12), the approximation in Eq. (14) adequately matches that of Eq. (8) provided

$$\{\eta_{\gamma}(1+R)\}^{-1} \ll (k_{\gamma}/\kappa_1) \ll J ; \qquad J(1+R) \simeq J' , \qquad (15)$$

notwithstanding that the number of terms in the double-sum in Eq. (14) is  $\{(2J+1) + (1+R)\}$  versus (2J'+1) in the single-sum in Eq. (8). However, the number of computational steps is  $\{(2J+1) \ (1+R)\}$  in Eq. (14) versus (2J'+1) in Eq. (8), which is in agreement with the second of Eq. (15) when J and J' >> 1. There is then no factorial saving in computational steps between Eq. (14), as it stands, and Eq. (8); using

one or the other equation is merely a matter of convenience. The crux of the report is revealed when one or the other factors composing  $F(k,\omega)$ ,  $K(k,\omega)$ , etc. is aliased in (k) with respect to  $(\kappa_1)$ , and  $(\kappa_1)$  matches the  $(\kappa_1)$  in Eq. (10a). Under this condition, a factorial saving of computational steps may be accrued by an appropriate manipulation of the integrand. A few examples in this regard are considered next.

### III. INTEGRAND COMPOSED OF ALIASED FACTORS

The expression depicted in Eq. (11) is specialized in that the factor  $K(k,\omega)$  is assumed to be aliased in (k) with respect to  $(\kappa_1)$ . [cf. Eq. (3).] Using the properties of the self-aliased operator  $S_b(k)$  as defined in Eq. (3), the integrand in Eq. (10a) can be equivalently expressed in form

$$S_b(k) \{exp(-ixk) \ K(k,\omega) \ G(k,\omega)\} \equiv K(k,\omega) \ S_b(k) \{exp(-ixk) \ G(k,\omega)\},$$
 if

$$K(k,\omega) = K(k+\kappa_j,\omega)$$
 (16a)

In terms of the approximation stated in Eq. (14), the "R-summand" equivalence assumes the form

$$S_b^J(k_r) \{exp(-ixk_r) \ K(k_r,\omega) \ G(k_r,\omega)\} \Rightarrow K(k_r,\omega) \ S_b^{J_1}(k_r) \{exp(-ixk_r) \ G(k_r,\omega)\};$$

$$k_{M1} = J_1 \kappa_1 , \qquad (16b)$$

where  $k_{M1}$  is the overall wavenumber span with respect to the convergence of the operand under  $S_b^{J_1}(k_r)$  in this equation and in general

$$S_b^{J_\beta}(k_r) \{N(k_r, \omega)\} = \sum_{j=-J_\beta}^{J_\beta} N(k_r + \kappa_j, \omega) . \qquad (12b)$$

It is noted that if the right side of Eq. (16b) is used in Eq. (14) instead of the left, a factorial saving equal to the smaller of  $(2J_1+1)$  and (2J+1) of computational steps is accrued. Usually, however,  $J_1 = J$  and, therefore, the two factors are equal. Moreover, if the aliasing in  $K(k,\omega)$  can be cast in the form

$$K(k,\omega) = S_h(k) \{K_A(k,\omega) \ K_B(k,\omega)\}, \qquad (17a)$$

then in terms of the approximation stated in Eq.(14), the R-summand equivalence becomes

$$S_b^J(k_r) \{exp(-ixk_r) \ K(k_r, \omega) \ G(k_r, \omega)\}$$

$$\Rightarrow S_b^{J_2} \{K_A(k_r, \omega) \ K_B(k_r, \omega)\} \ S_b^{J_1}(k_r) \{exp(-ixk_r) \ G(k_r, \omega)\};$$

$$k_{M2} = (J_2\kappa_1), \qquad (17b)$$

where  $k_{M2}$  is the overall wavenumber span with respect to the convergence of the operand  $\{K_A(k,\omega) \mid K_B(k,\omega)\}$  under  $S_b^{J_2}(k)$ . It is noted that the factorial saving of computational steps pertaining to Eq. (17b) remains unchanged from that derived from Eq. (16b). If, in addition to the form of  $K(k,\omega)$ , as stated in Eq. (17a), it is assumed that

 $K_A(k,\omega)$  is aliased in (k) with respect to  $(\kappa_1)$ , then the factor  $K(k,\omega)$  can be factorized further in the form

$$K(k,\omega) = K_A(k,\omega) S_b(k) \{K_B(k,\omega)\}, \text{ if}$$
 
$$K_A(k,\omega) = K_A(k+\kappa_i,\omega). \tag{18a}$$

In terms of the approximation stated in Eq. (14), the R-summand equivalence assumes the additional factorization, over Eq. (17b), of the form

$$S_b^J(k_r) \{exp(-ixk_r) \ K(k_r, \omega) \ G(k_r, \omega)\}$$

$$\Rightarrow K_A(k_r, \omega) \ S_b^{J_3}(k_r) \ K_B(k_r, \omega)\} \ S_b^{J_1}(k_r) \{exp(-ixk_r) \ G(k_r, \omega)\};$$

$$k_{M3} = (J_3\kappa_1), \qquad (18b)$$

where  $k_{M3}$  is the overall wavenumber span with respect to the convergence of the quantity  $K_B(k,\omega)$  in this equation. It is noted that if in Eq. (14) the right side of Eq. (18b) is used instead of that of Eq. (16b), a factorial saving equal to the smaller of  $(2J_2+1)$  and  $(2J_3+1)$  of computational steps is accrued. Usually, however,  $J_{\beta}=J$  and, therefore, the two factors are equal. Under this equality, it is noted that if the right side of Eq. (18b) is used in Eq. (14) instead of the left, a factorial saving of  $(2J+1)^2$  of computational steps is accrued. In the event that the aliasing in the factor  $K_A(k,\omega)$ , as stated in Eq. (18a), stems from its functional dependence on an aliased quantity; e.g.

$$K_A(k,\omega) = K_A[S_b(k) \{K_{AA}(k,\omega)\}],$$
 (19a)

the approximation stated in Eq. (14) supports the R-summand equivalence of the form

$$\begin{split} S_b^{J}(k_r) \; & \{ exp(-ixk_r) \; \; K(k_r, \omega) \; \; G(k_r, \omega) \} \\ & \Rightarrow \; K_A^{J_4}(k_r, \omega) \; \; S_b^{J_3}(k_r) \; \{ K_B(k_r, \omega) \} \; \; S_b^{J_1}(k_r) \; \{ exp(-ixk_r) \; \; G(k_r, \omega) \} \; \; ; \end{split}$$

$$K_A^{J_4}(k_r,\omega) = K_A[S_b^{J_4}(k_r) \{K_{AA}(k_r,\omega)\}]; \qquad k_{M4} = (J_4\kappa_1),$$
 (19b)

where  $k_{M4}$  is the overall wavenumber span with respect to the convergence of the quantity  $K_{AA}(k,\omega)$  in this equation. It is noted that there is no factorial saving of computational steps between the use of Eqs. (18b) and (19b). If further factorization exists, either in  $K_A(k,\omega)$ , in  $K_B(k,\omega)$  or in both, in the format just prescribed, one may gain more and more factorial savings. For the purpose of this report, however, the factorization and dependence considered in Eqs. (18a) and (19a) suffice.

A special case of Eq. (11) is that in which, in addition to the aliasing of  $K(k,\omega)$  in (k) with respect to  $(\kappa_1)$ , the function  $G(k,\omega)$ , in this equation, is independent of the wavenumber (k); namely

$$F(k,\omega) = G_o(\omega) K(k,\omega) ; K(k,\omega) = K(k+\kappa_j,\omega) . (20)$$

Substituting Eq. (20) in Eq. (10a) derives

$$f(x,\omega) = s_b(x) \{\delta(x) \ f_s(x,\omega)\};$$

$$f_s(x,\omega) = [G_o(\omega)/\kappa_1] (2\pi)^{-1/2} \int_0^{\kappa_1} dk \exp(-ixk) K(k,\omega) ,$$
 (21)

where  $s_b(x)$  is a self-aliased spatial (x) operator with respect to the fundamental separation distance (b);  $b=(2\pi/\kappa_1)$ . This operator is defined

$$s_b(x) \{n(x,\omega)\} = \sum_j n(x+x_j,\omega) ; \qquad x_j = (jb) ; \qquad x_o = 0 .(22)$$

[cf. Eq. (3).] Executing the integral in Eq. (21) in a manner analogous to that resulting in Eq. (14), one obtains

$$f_s(x,\omega) = (2\pi)^{-1/2} [G_o(\omega)/(1+R)] \sum_{r=0}^{R} \{exp(-ixk_r) | K(k_r,\omega)\},$$
 (23)

and the evaluation of  $f_s(x,\omega)$  is considered, in view of Eq. (21), to be synonymous with the evaluation of  $f(x,\omega)$ , notwithstanding the acknowledgment that, unlike  $f(x,\omega)$ , the evaluation of  $f_s(x,\omega)$  is meaningful only for values of  $x=x_j$ ;  $x_j=(jb)$ . In this view, the recognition of the aliasing in  $K(k,\omega)$ , as stated in Eq. (20), is worth a factorial saving of (2J+1) of computational steps. This is similar to the factorial saving that is accrued in Eq. (16b), utilizing the same recognition. Indeed, the factorization of  $K(k,\omega)$ , as depicted in Eqs. (16) - (19) and beyond, are just as beneficial with respect to Eq. (23) as they are with respect to Eq. (14).

### REFERENCES

- 1. L. Cremer, M. Heckl, and E. Ungar, <u>Structure-Borne Sound</u>, <u>Structural Vibrations</u> and <u>Sound Radiation at Audio Frequencies</u>, (Springer-Verlag, 2nd Ed., 1988).
- 2. G. Maidanik and J. Dickey, "Velocity distributions on unloaded finitely and regularly ribbed membranes," J. Acoust. Soc. Am., 149, 43-70 (1991) and "Response of regularly ribbed fluid loaded panels," J. Acoust. Soc. Am., 155, 481-495 (1992).
- 3. G. Maidanik and J. Dickey, "Quadratic and energy estimates of the partial response of ribbed panels," J. Acoust. Soc. Am., 94, 1435-1444 (1993) and "Influence of variations in loss factor of a panel and line impedance of attached ribs," J. Acoust. Soc. Am., 94, 1445-1452 (1993).
- 4. G. Maidanik and J. Dickey, "Localization and delocalization in periodic one-dimensional dynamic systems," Acustica, <u>73</u>, 119-128 (1991).
- 5. C.B. Burroughs, "Acoustic radiation from fluid-loaded infinite circular cylinders with doubly periodic ring supports," J. Acoust. Soc. Am., 75, 715-722 (1984).
- 6. M.C. Junger and D. Feit, <u>Sound, Structures, and Their Interaction</u>, (MIT Press, 1986).
- 7. F. Fahy, <u>Sound and Structural Vibration (Radiation, Transmission and Response)</u>, (Academic Press, 1985).
- 8. M.P. Norton, <u>Fundamentals of Noise and Vibration Analysis for Engineers</u>, (Cambridge University Press, 1989).
- 9. G. Maidanik and K.J. Becker, "Use of the double-sum technique for computing the modal response of regularly ribbed cylinders," NSWCCD SIG-96/061-7030 (1996).
- G. Maidanik and K.J. Becker, "Phenomena of aliasing and pass and stop bands in the drive in lieu of ribs on cylindrical shells," NSWCCD report no. SIG-96/072-7030 (1996).

- 11. K.J. Becker, "On the response of regularly ribbed cylindrical shells," thesis in preparation.
- 12. R.J. Mayhan, <u>Analysis of Discrete-Time and Continuous-Time Linear Systems</u>, (Addison-Wesley, 1984).

### INITIAL DISTRIBUTION

Copies		Copies			
3	NAVSEA 03T2 2 Taddeo 1 Becker	1	Penn State University 1 Koopman		
4	ONR/ONT 1 334 Vogelsong 1 334 Tucker	2	Virgin 1 1	nia Tech Knight Fuller	
	1 334 Main 1 Library	(	CENTE	ER DISTRIBUTION	
4	NRL	Copies	Code	Name	
	1 5130 Bucaro 1 5130 Williams	1	011		
	1 5130 Photiadis 1 Library	1	0112 0112	Douglas Halsall	
4	NUWC/New London 1 Sandman	1	20		
	1 Harari 1 3332 Lee	1	204		
	1 Library	1	2040	Everstine	
1	NUWC/NPT Library	1	2042 2042	Hambric	
2	DTIC	1	70		
1	Johns Hopkins University Green	1	7030		
1	Applied Physics Lab	1	7200	Hwang	
4	Johns Hopkins University Library	1 1 1	7250 7250 7250	Maga Vasudevan	
4	ARL/Penn State University 1 Biancardi 3 Burroughs	1	726	Szilagyi	
1		1	804.1	Dickey	
1	Cambridge Collaborative Manning	2	3421	(TIC-Carderock)	
1	Georgia Tech/M.E. Dept. Ginsberg				
1	MIT Dyer				